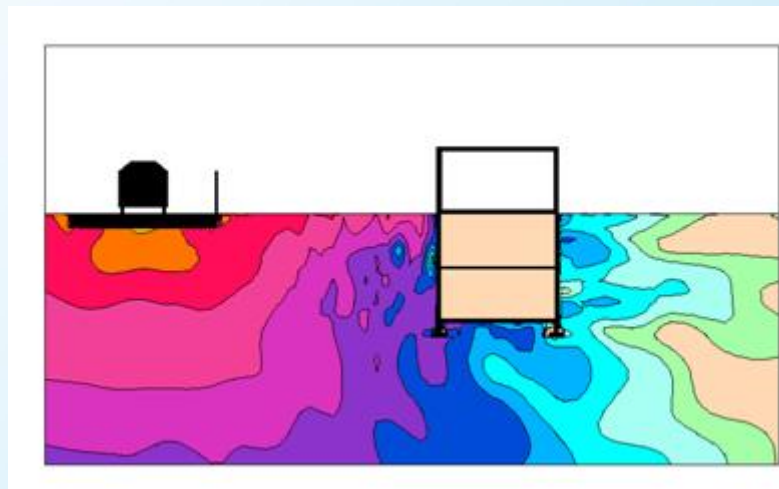
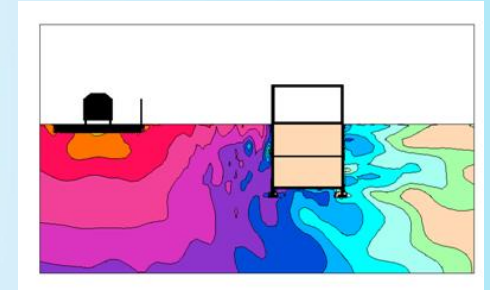


# Numerical tools to model ground/structure interaction (+ Track system modeling and testing)

Philippe JEAN, Michel VILLOT



# Introduction



## Problem

source : model calibration from ground vibration

Propagation: ground models

Transfer to structure: type of contact, 2D, 3D

Propagation through structures

Acoustic radiation in rooms

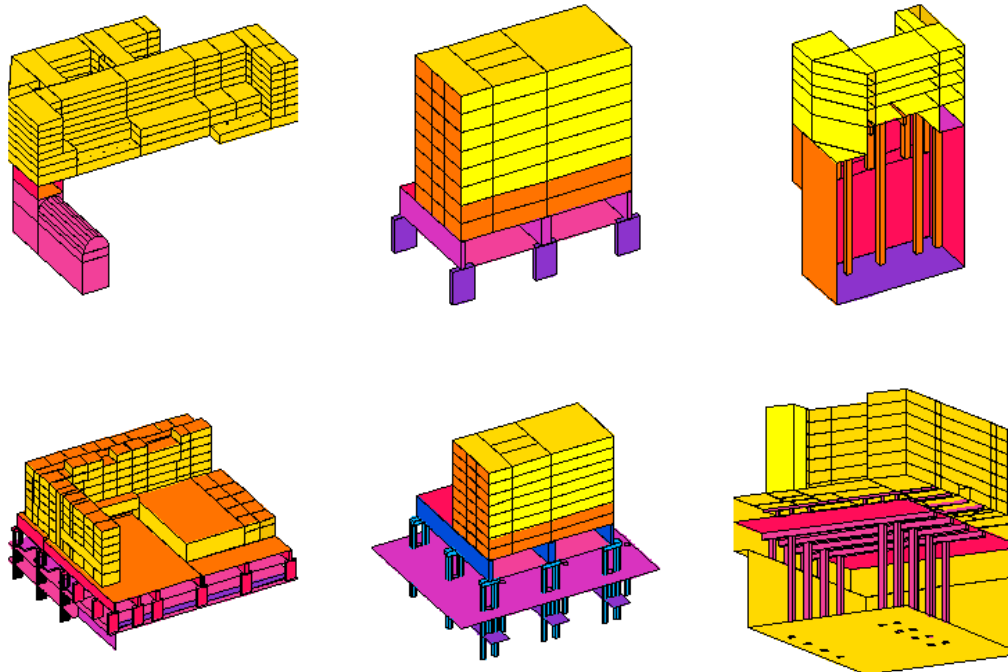
Perception : vibration, ground borne noise

Exposure descriptors

**Modèles:** Energetic, FEM/BEM, hybrid, mobilities,..

# (SEA) Statistical Energy Analysis

Linked to other models for  
underground structures



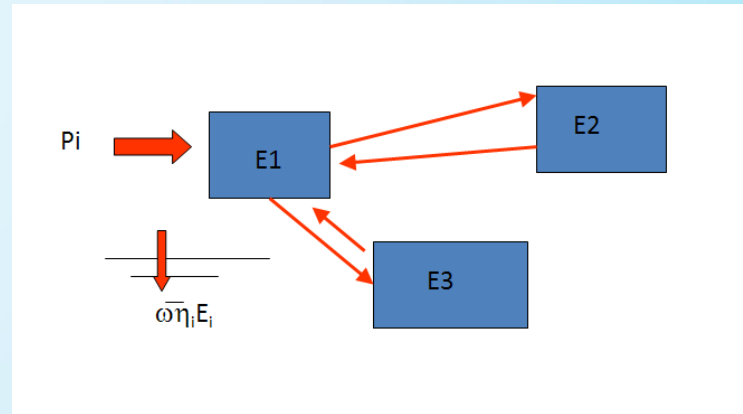
# SEA : Principles

Decomposition of the problem into systems: plates/ beams/ columns

Average Energies (F,L,T) per system & per bandwidth (1/3 octave)

Power balance

$$P_i = \omega \eta_i E_i + \sum \omega \eta_{ij} (E_i / n_i - E_j / n_j)$$



$$\begin{pmatrix} \eta_{1+} & -\eta_{21} & -\eta_{31} \\ \eta_{12+} & & \\ \eta_{13} & & \end{pmatrix} \begin{pmatrix} E1 \\ E2 \\ E3 \end{pmatrix} = \begin{pmatrix} P_i/\omega \\ 0 \\ 0 \end{pmatrix}$$

## SEA : limitations

Minimum of modes per bandwidth required

Problem in Low Freq for longitudinal waves:

In practice:

- OK for bending excitation down to 50 Hz
- NO for in plane excitation

⇒ Hybrid Models SEA/ modal / waves

Models adapted to Low Frequencies: FEM / BEM

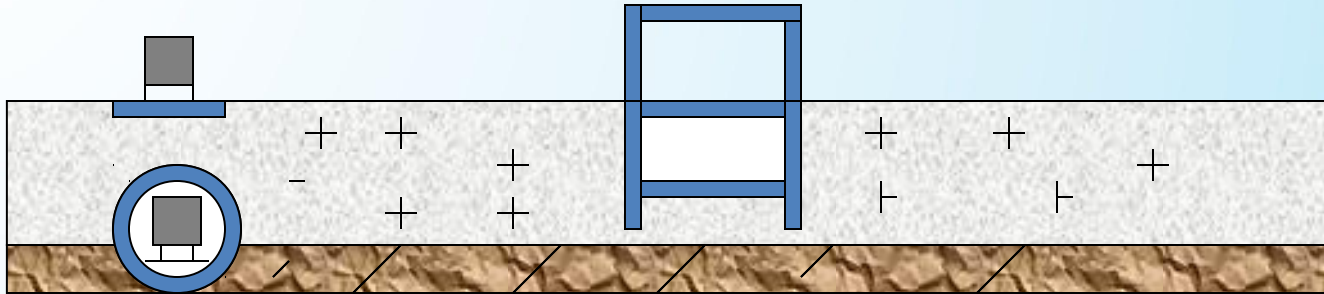
# FEM/BEM methods Software MEFISSTO



FEM : Finite Element Method  
BEM : Boundary Element method



## Interaction Grounds/Structures (2D & 2.5D)



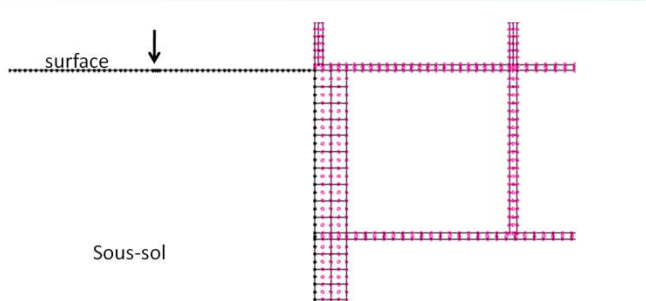
$$\bar{u}(M) \cdot \bar{I}(M) = \int_S [\bar{T}(Q, M) \cdot \bar{u}(Q) - \bar{G}(Q, M) \cdot \bar{t}(Q)] dS + \bar{h}(M)$$

- Separation into sub-domains
- Integral Representation BEM (collocation) (ground or thick structures)
- or FEM: condensation at boundaries (structure or portions of ground)
- Continuity of displacements and/or stresses at interfaces

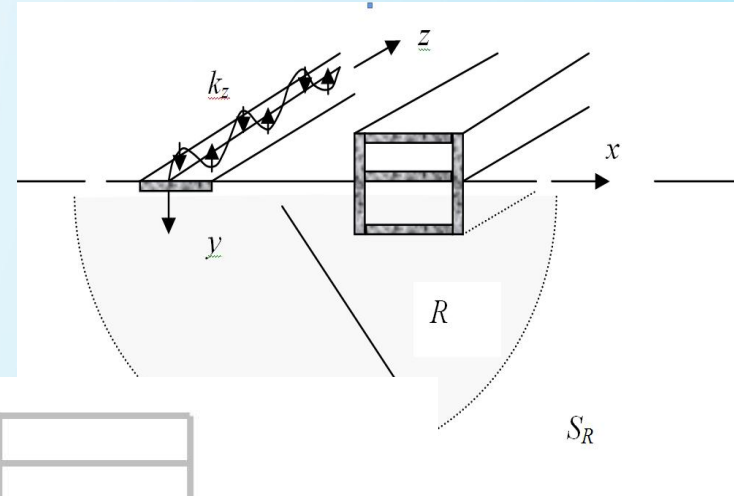


# FEM/BEM methods

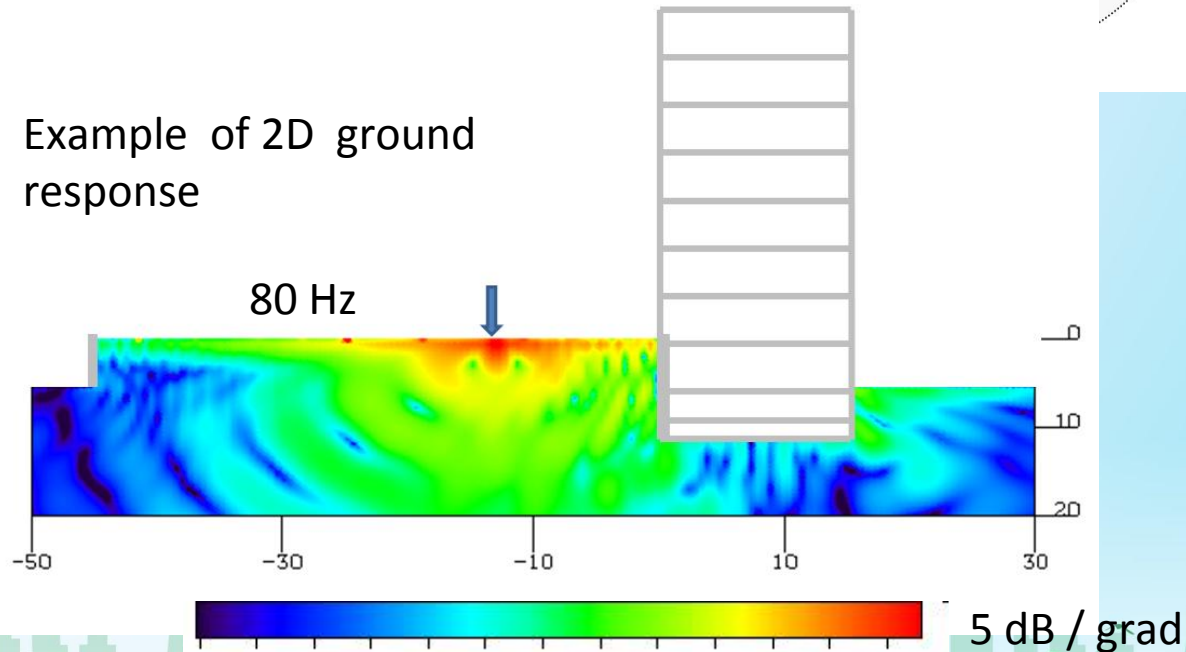
Example of 2D meshing



2.5D approach



Example of 2D ground response



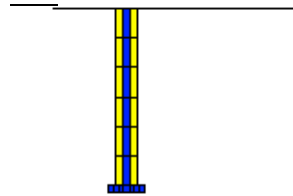


# Foundation ground lining (ADEME)

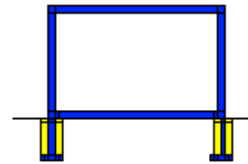
Cas A



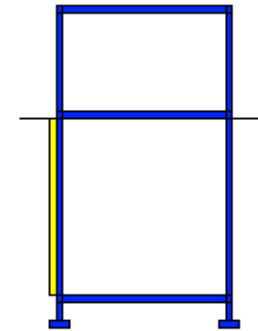
Cas C



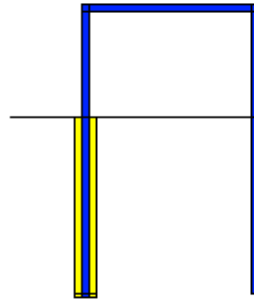
Cas E



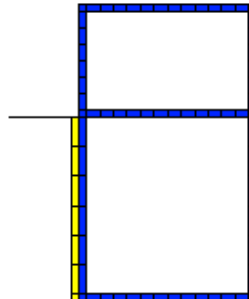
Cas G



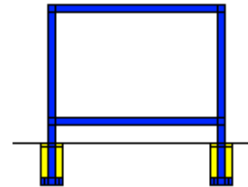
Cas B



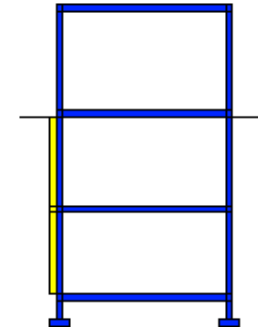
Cas D



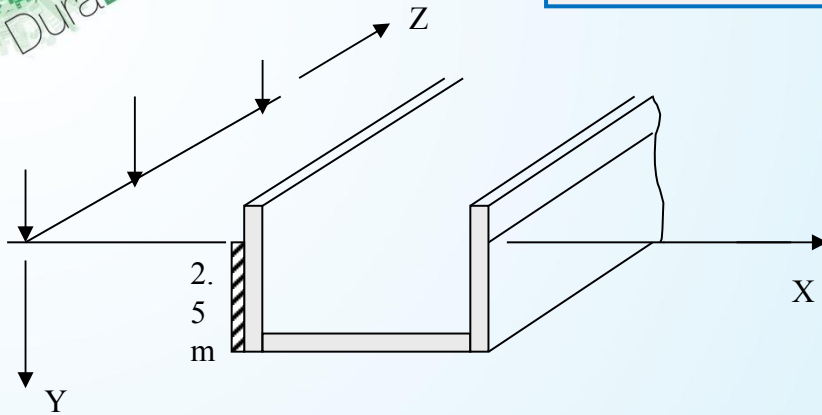
Cas F



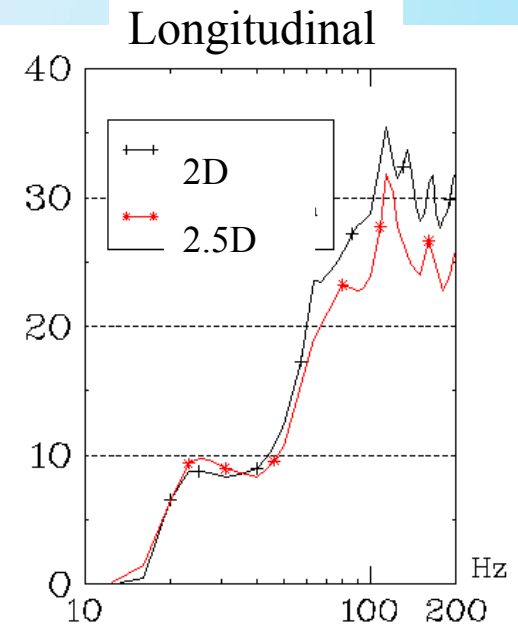
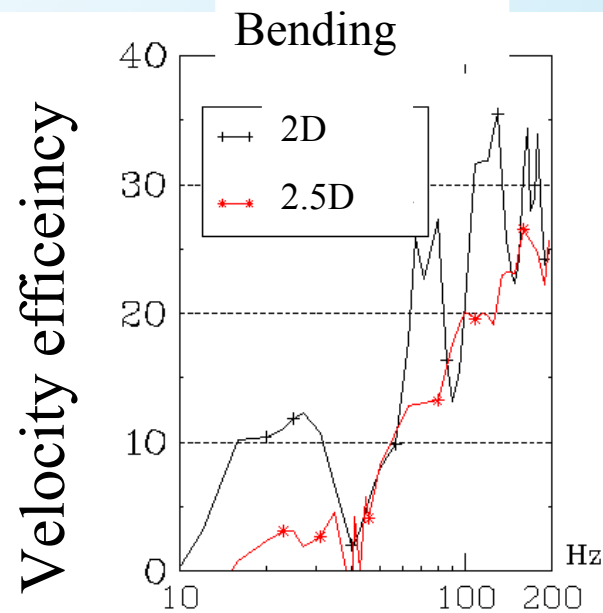
Cas H



## BEM 2.5D

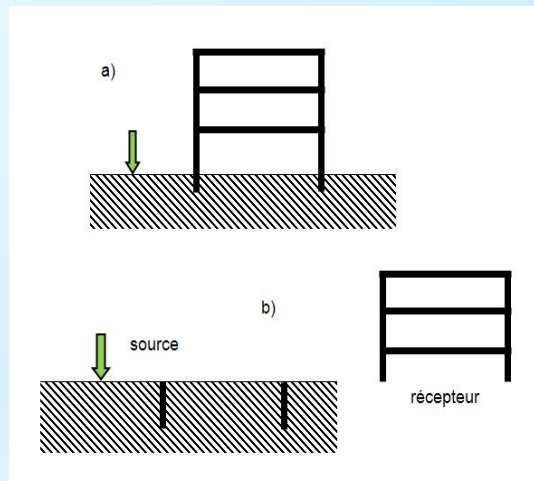


Example of calculated efficiency 2D / 2D  $\frac{1}{2}$

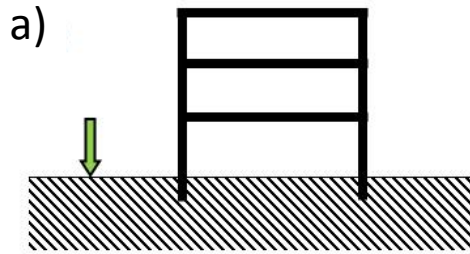


# Source Receiver Mobility Approach

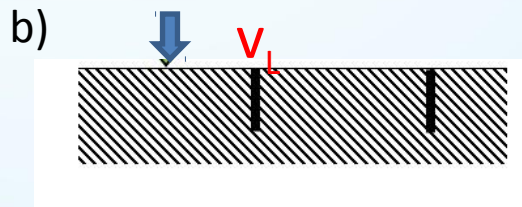
*PhD Pierre ROPARS (2009-2011)  
CSTB/ Univ Paris Est*



## PRINCIPLE

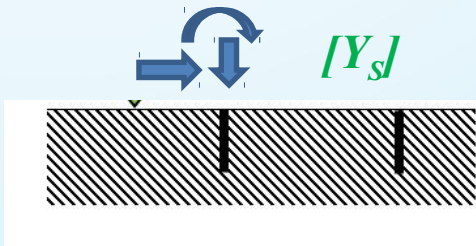


Separation of a problem into 2 parts  
 (a) / (b) : source/receiver

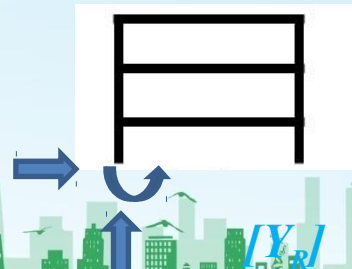


$$\text{Contact force } (f_c) = ([Y_S] + [Y_R])^{-1} (v_L)$$

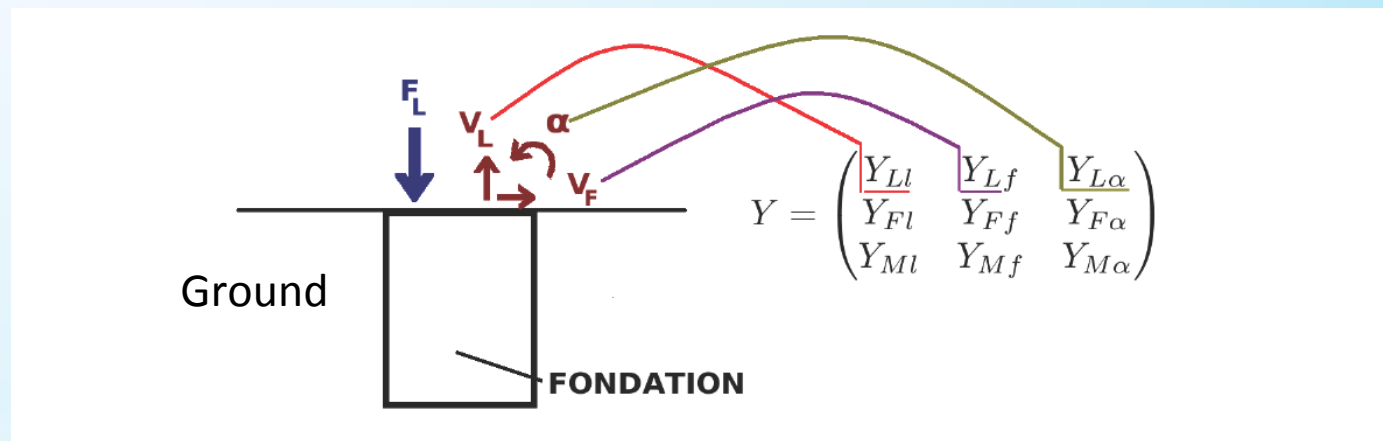
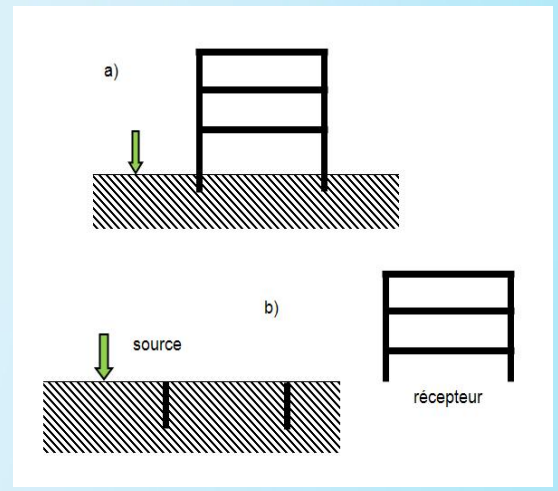
$$\text{Contact velocity } (v_c) = [Y_R] ([Y_S] + [Y_R])^{-1} (v_L)$$



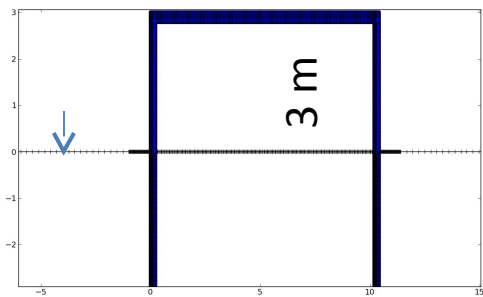
$$\text{Power into building } \Pi = 1/2 \operatorname{Re}\{ (f_c)^T (v_c)^* \}$$



Models used:  
 BEM/FEM (Mefissto) : ground + foundations  
 FEM (NASTRAN) : Buildings



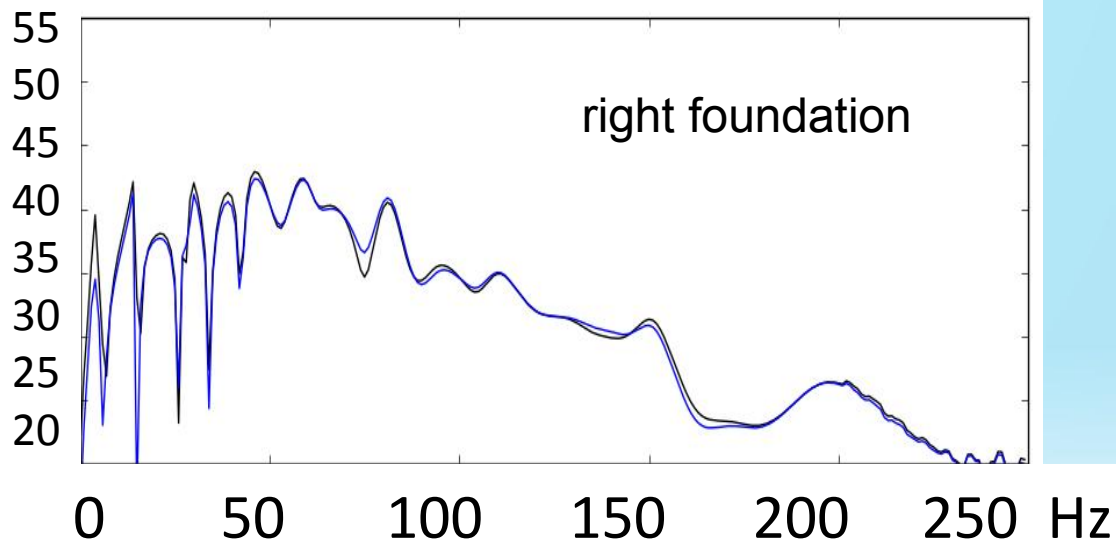
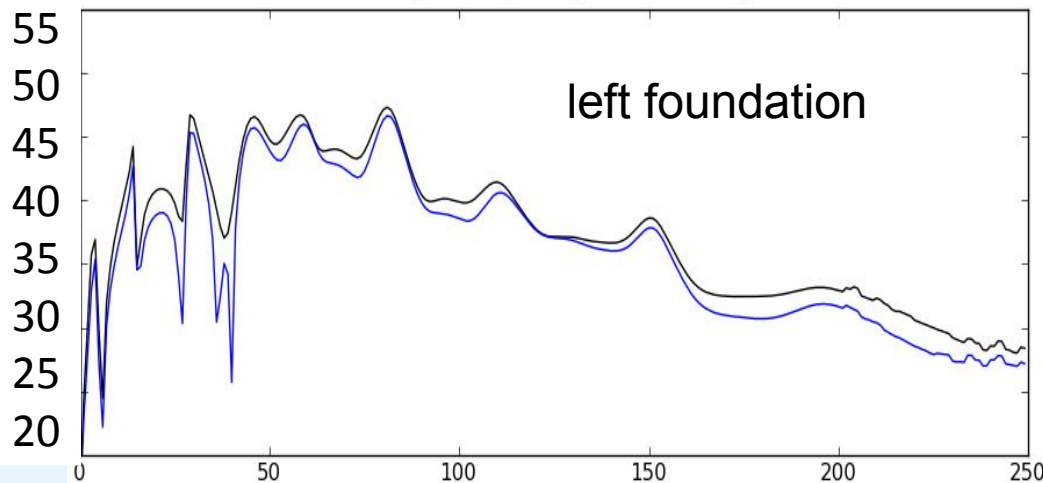
Mobility Technique: VALIDATION



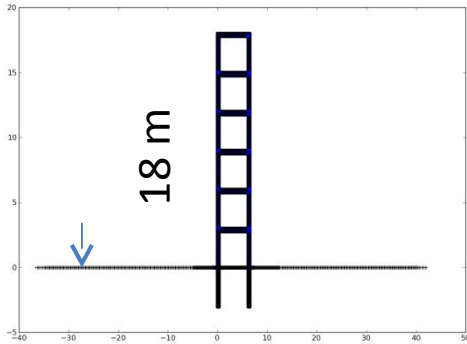
10 m

Total injected Power:  
**Mobility Approach**  
**MEFISSTO**

Real part of power[dB ref 10e-12]

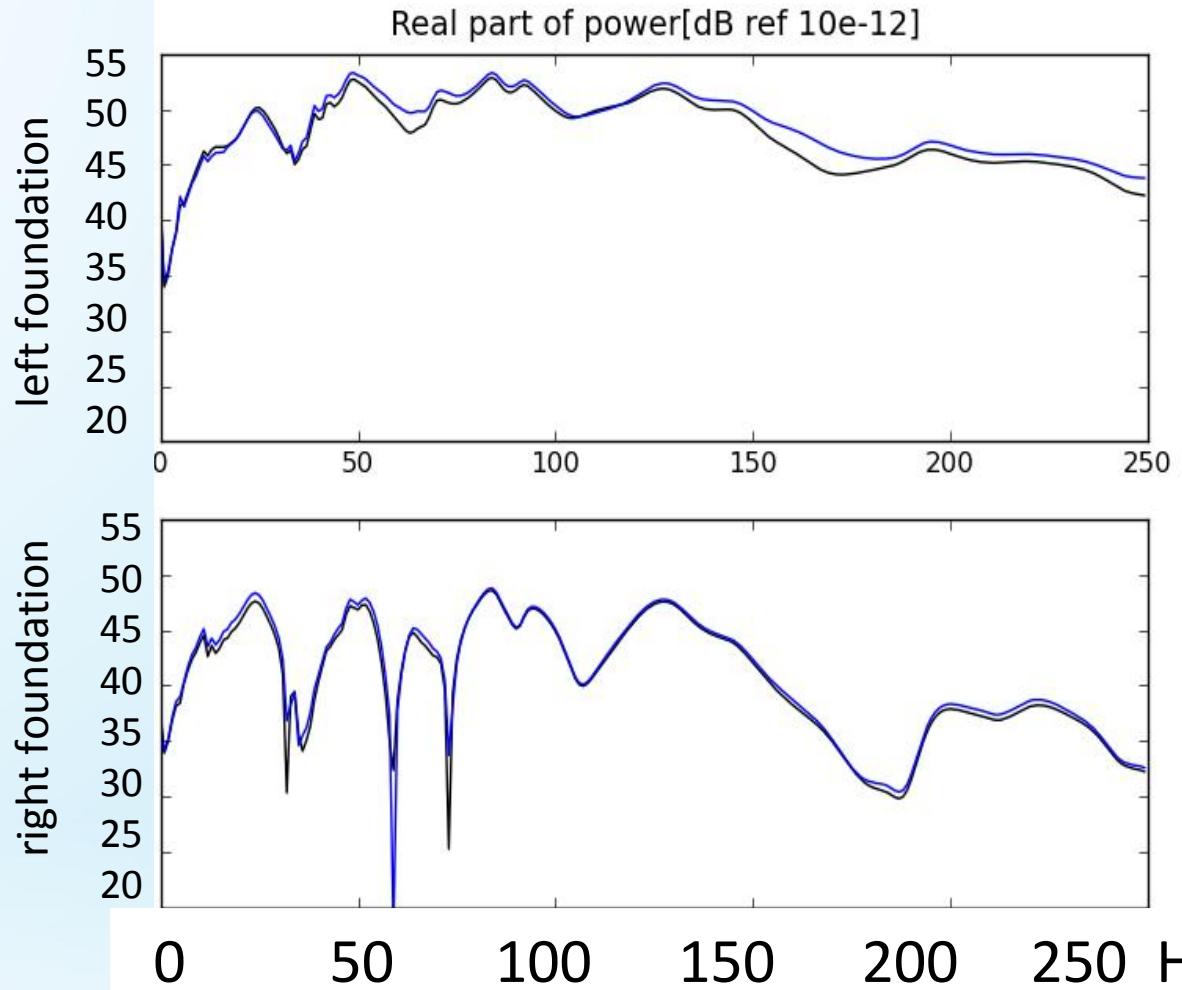


Mobility Technique: VALIDATION



10 m

Total injected Power:  
**Mobility Approach**  
**MEFISSTO**



Buildings close to  
Railway Tracks  
Validation + influence of  
structural modifications

VIBSOLFRET  
SNCF/CSTB/SATEBA



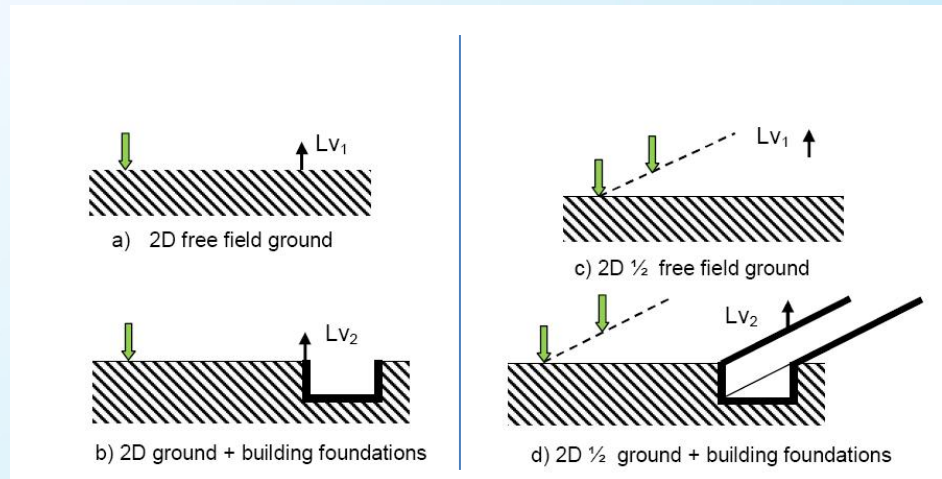


# VIBSOLFRET ; source calibration

SNCF/CSTB/SATEBA

1. Source calibrated from measured ground vibration
2. Transfer Function :  $H = LV(\text{ground only}) - LV(\text{ground+foundation})$

computed in 2D and 2D ½



3. Extrapolation to other situations: BEM2D computations:  
Calibration of 2D BEM computations corrected by :  $H(2D) / H(2.5D)$

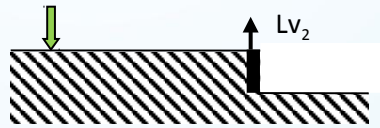
# Calibration correction factor 2.5D / 2D



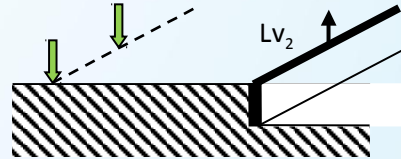
a) 2D free field ground



c) 2D 1/2 free field ground

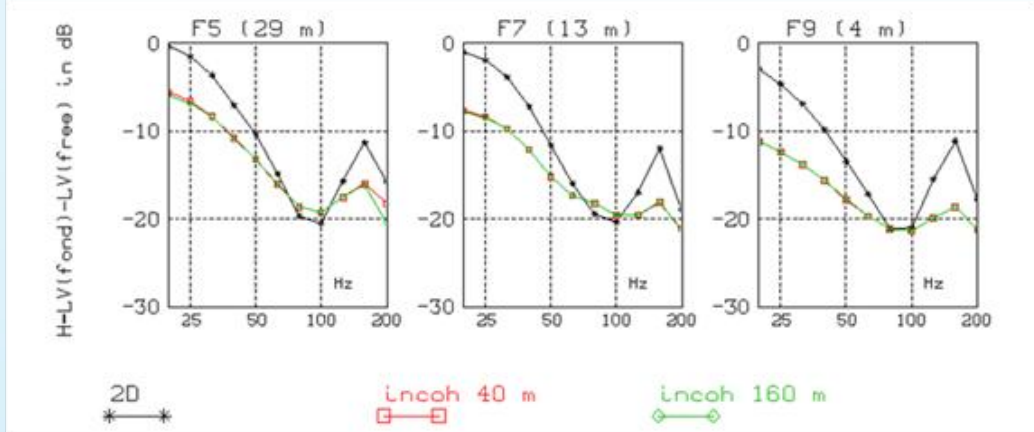


b) 2D ground + building foundations

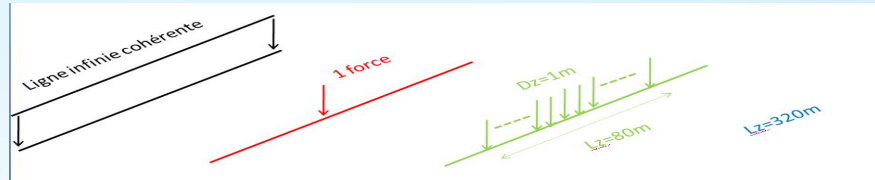


d) 2D 1/2 ground + building foundations

$$H = LV(\text{ground}) - LV(\text{foundation})$$



Coherent line, point source forces every meter along 80 m, along 320 m



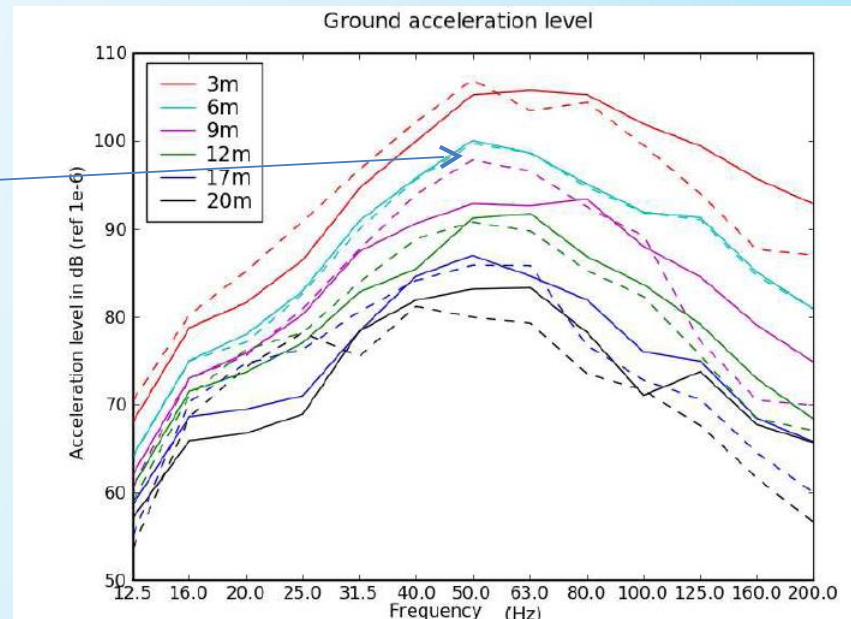
# VIBSOLFRET ; ground calibration

SNCF/CSTB/SATEBA

Surface Acceleration at d m to the track  
BEM2.5D referenced to d=6 m

- Use of 3 types of homogeneous ground
- standard
  - rather hard
  - rather soft

Ground evaluated by comparing  
calculated and measured attenuation  
spectra

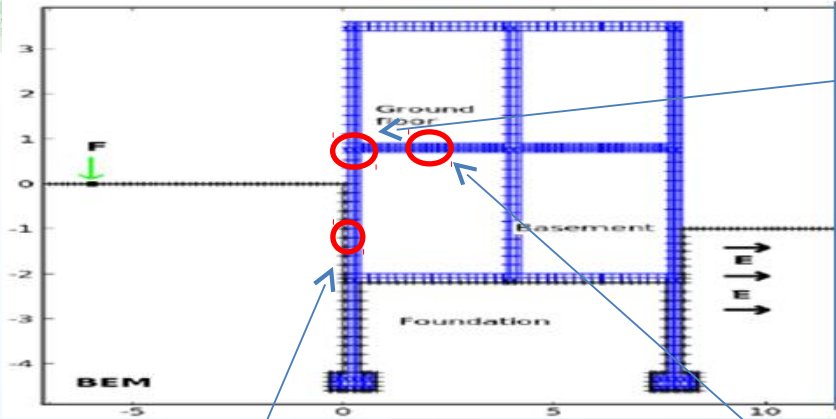


Attenuation with distance:  
MEFISSTO 2.5D (\_\_\_) measured (- - -)

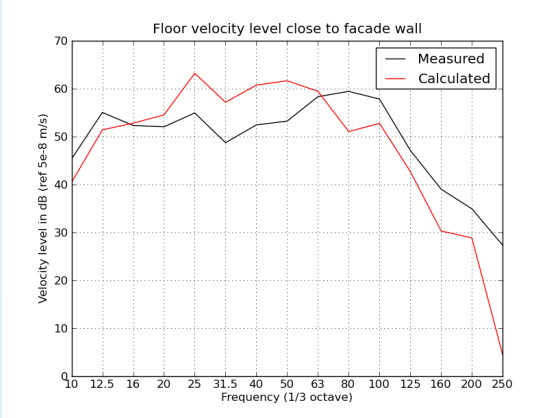


# VIBSOLFRET ; experimental validation

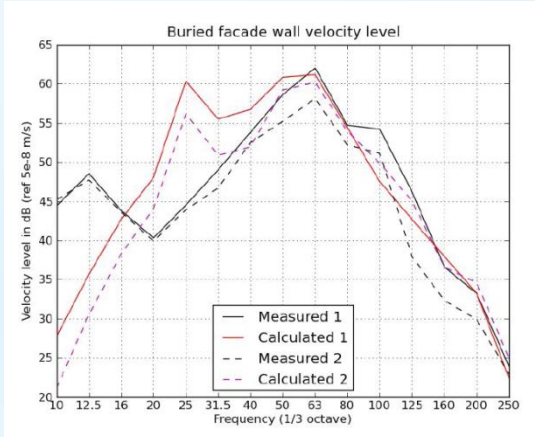
## SNCF/CSTB/SATEBA



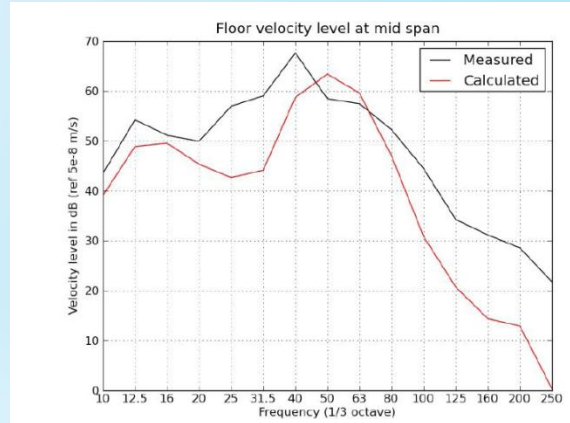
Measured  
Computed



Vertical velocity on the facade



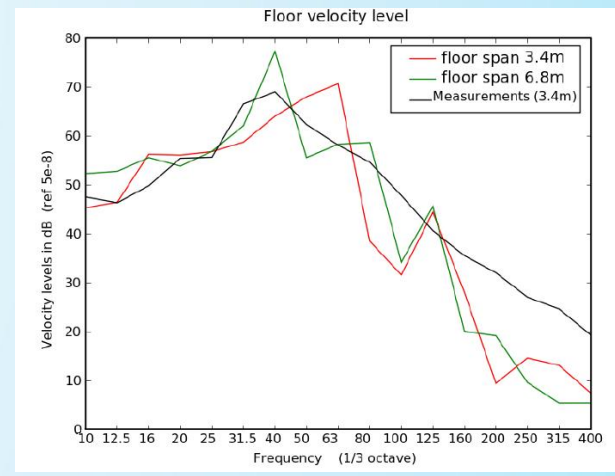
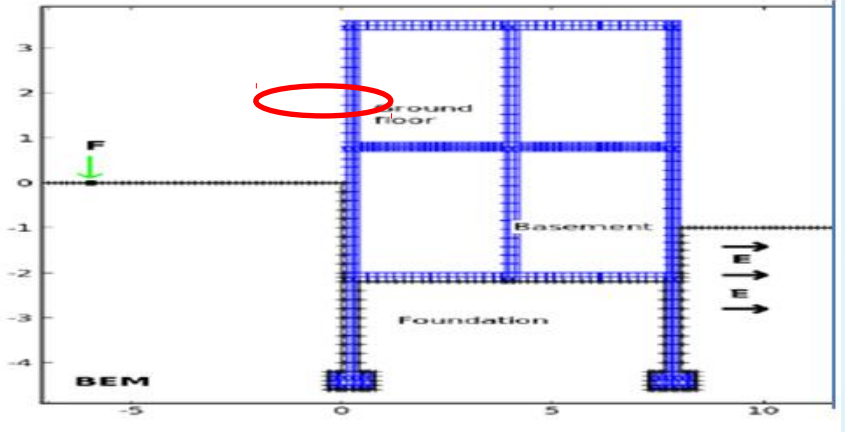
Horizontal Velocity: burried front wall



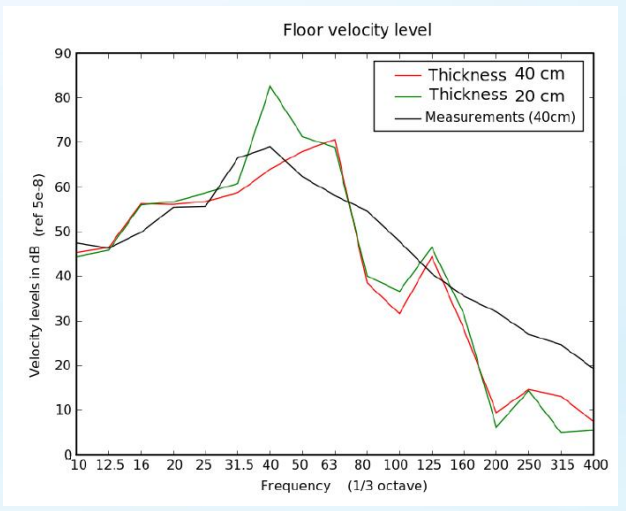
Bending Velocity on floor (Centre)

# VIBSOLFRET ; influence of structural modifications

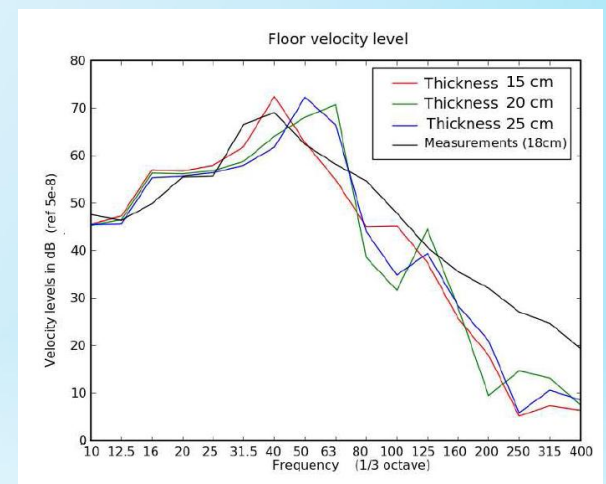
## SNCF/CSTB/SATEBA



Influence of floor dimension



Influence of facade thickness



Influence de floor thickness



# VIBSOLFRET ; vibration descriptors

SNCF/CSTB/SATEBA

Descriptors for annoyance (e.g. Norwegian standard NS 8176) integrated into the numerical model

Measured situation:

dist to tracks=6m, h facade=40cm, h floor=20cm, floor length=3.4 m

Indicator  $V_{w,95}$  for simulated situations

	Measure d (6 m)	Same Building at 20 m	h facade 20 cm	h floor 15 cm	h floor 25 cm	Floor length= 6.80m
$v_{w,95}$ mm/s	0.11	0.04	0.89	0.26	0.11	0.56

**Class A** ( $v_{w,95} < 0.1$ ): vibrations non perceived

**Class B** ( $0.1 < v_{w,95} < 0.15$ ): low % of annoyance (<10%) likely to occur

**Class C** ( $0.15 < v_{w,95} < 0.3$ ): about 15% of people annoyed (recommended for new buildings)

**Class D** ( $0.3 < v_{w,95} < 0.6$ ): about 25% of annoyance likely to occur

(recommended for existing buildings if upgrading costs to reach class C are too high)



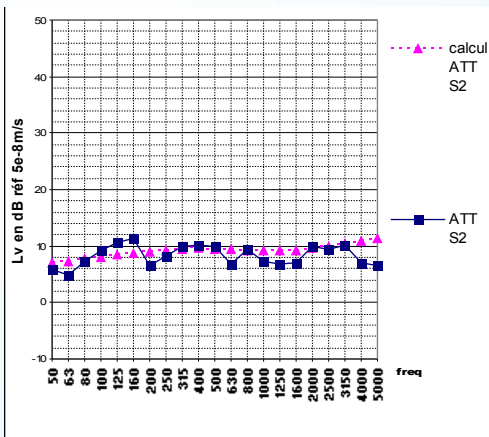
Sources inside buildings:

Drills, impact hammer... (bending excitation)

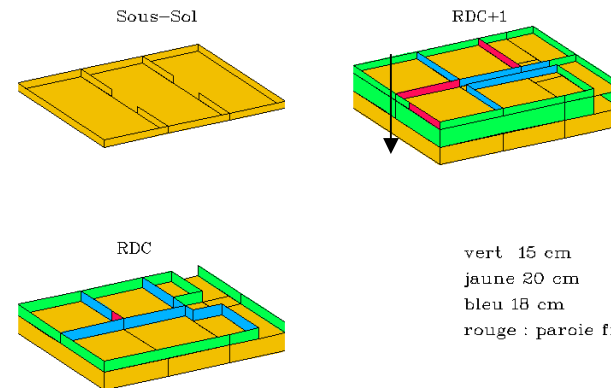
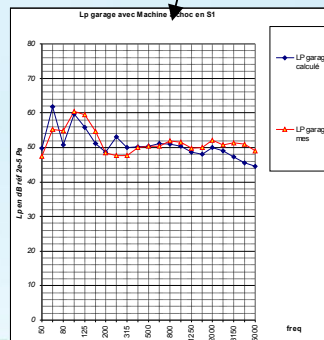
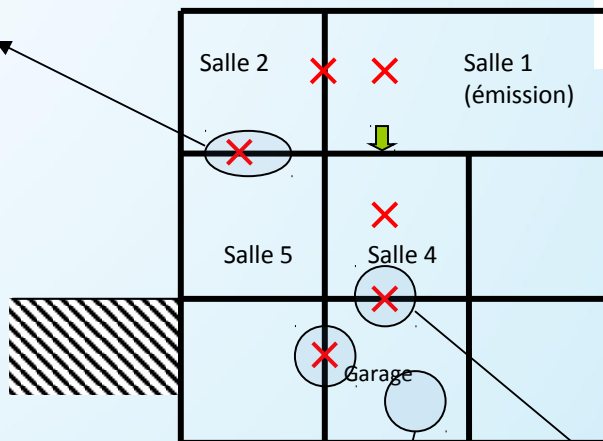
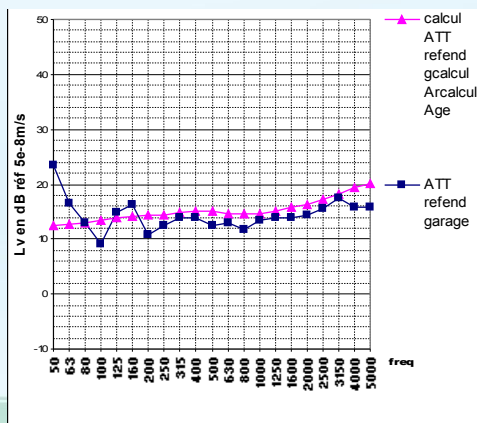
BOUYGUES/CSTB



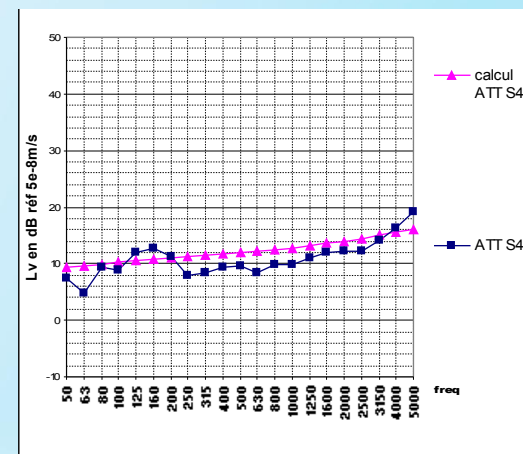
## Velocity Levels



## Velocity Levels



## Velocity Levels



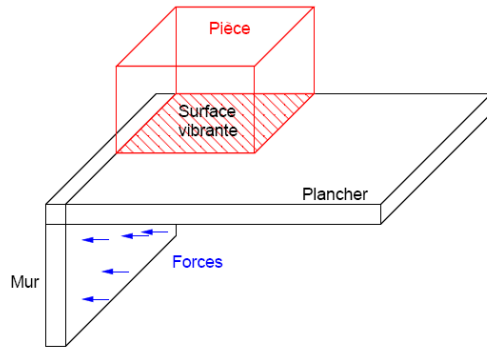
## Sound Levels



# Acoustic Radiation into rooms

## Computations

PhD Guillaume COCQUEL (2005-2008) RATP/CSTB



$$\sigma = \frac{\Pi_{rad}}{\rho_0 c_0 S \langle v^2 \rangle} \quad \text{where} \quad \Pi_{rad} = \frac{\langle p^2 \rangle A}{4 \rho_0 c_0}$$

### Modelisation of Acoustic Radiation

Analytical model => floor velocity V

Acoustic Radiation: V, G (room response) => P

$$p(M) = \int_{S_v} j\omega\rho_0 \times v(Q) \times G_v(M, Q) \times dS(Q)$$

Tr => A    A et P<sup>2</sup> =>  $\Pi_{rad}$  =>  $\sigma$

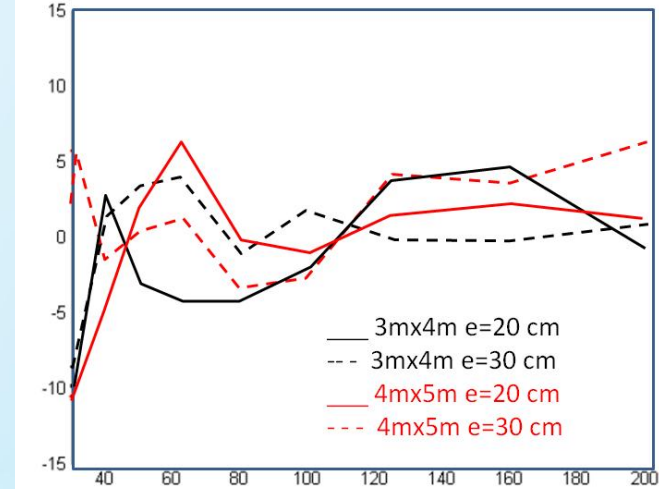
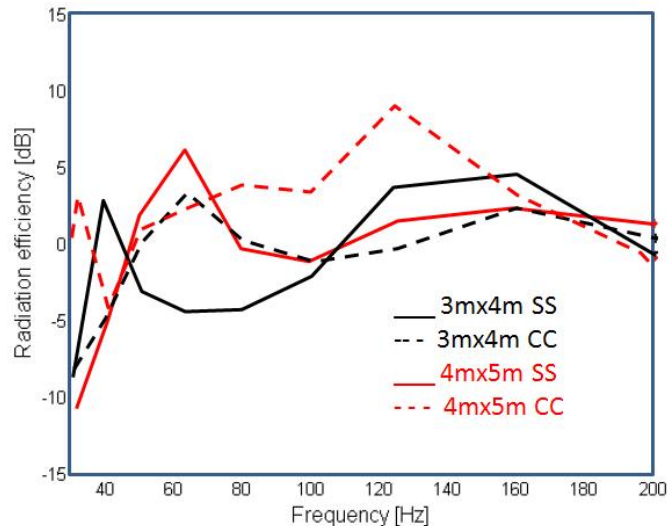
# Effect of characteristics on the radiation factor

2 dimensions 3x4 m<sup>2</sup> & 4x5 m<sup>2</sup>

2 boundary conditions: simply supported (SS) & clamped (CC)

2 thicknesses : 20 cm & 30 cm

## Example of calculated radiation efficiency

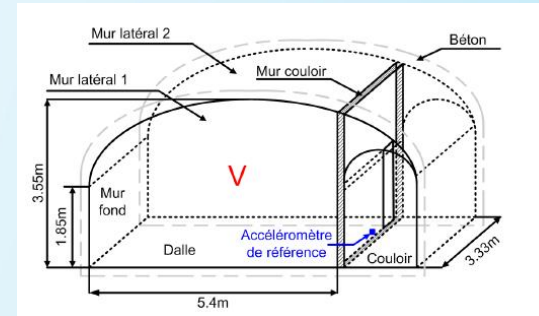


=> Estimation of uncertainty range



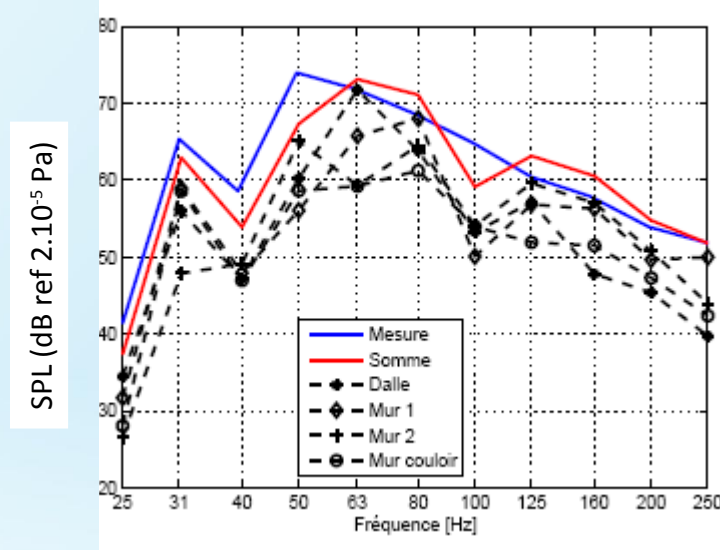
# Acoustic Radiation into volumes: measurements

*Technical Room at RATP*



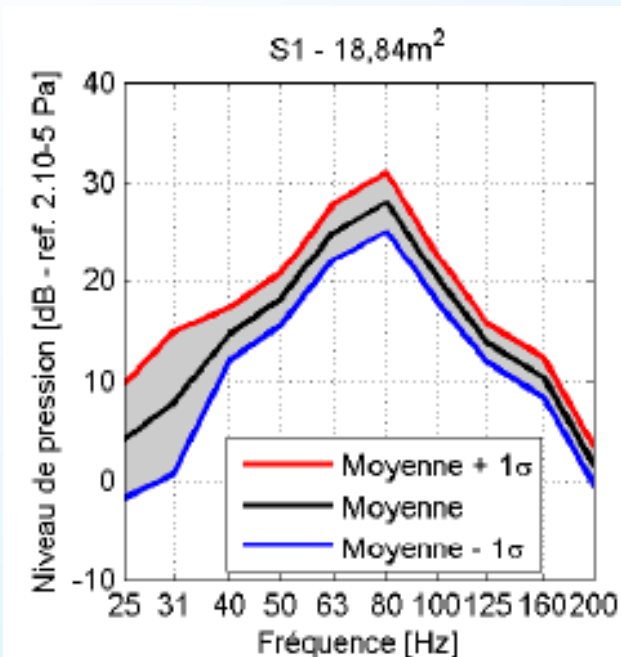
Measurement of  $L_v$  (floor and walls)

Estimation of sound from  $L_v$  and  
calculated radiation efficiency  
 $\sigma$  et  $Tr \Rightarrow \Pi_{rad} \Rightarrow LP$

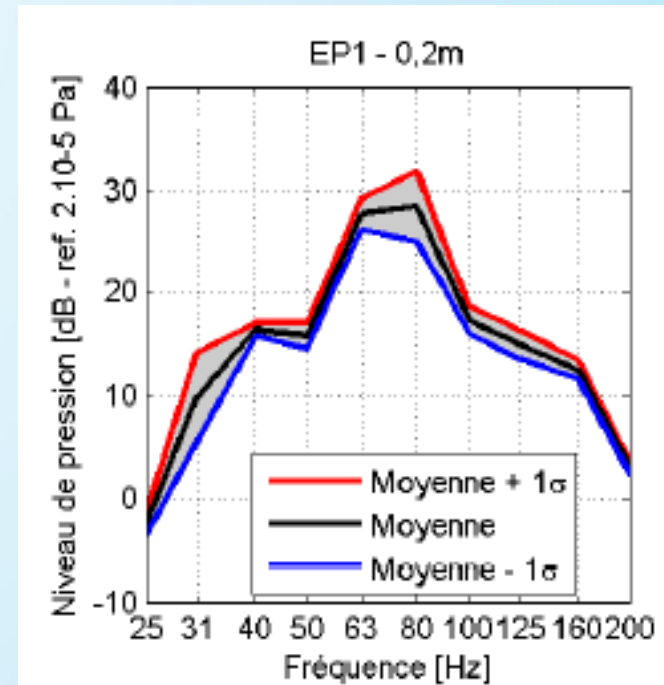


# Acoustic Radiation into volumes: variability

Computed variability : mean value and standard deviation



Blocked floor dimensions



Blocked floor thickness

- Salle de séjour : S1 = 18,24m<sup>2</sup>, S2 = 19,11m<sup>2</sup>, S3 = 20,00m<sup>2</sup>, S4 = 20,91m<sup>2</sup>, S5 = 21,84m<sup>2</sup>,
- Hauteur : H1 = 2,5m, H2 = 2,6m, H3 = 2,7m, H4 = 2,8m, H5 = 2,9m, H6 = 3m,
- Epaisseur de la dalle : EP1 = 0,200m, EP2 = 0,225m, EP3 = 0,250m, EP4 = 0,275m, EP5 = 0,300m,
- Conditions aux limites : Encasté (CC), Appuis Simples (SS).

# Track work: model

## Track system modeling:

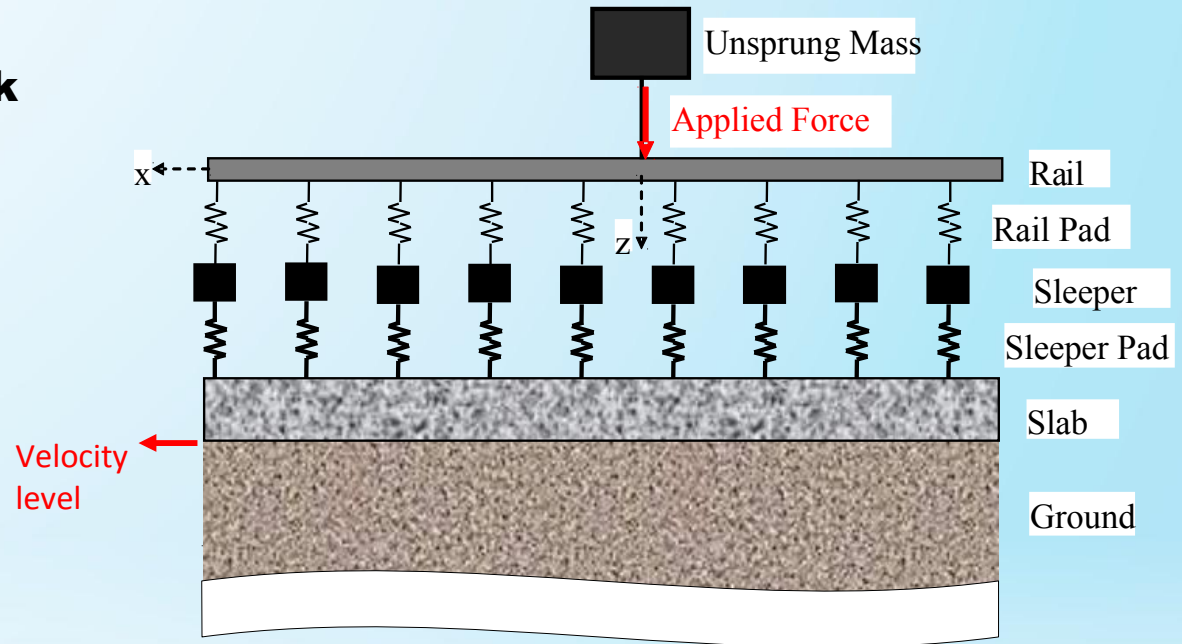
- **CASC software based on wave approach on infinite beam structures**

- **comparison between track systems (insertion gain)**

- **laboratory test rig optimization**

Output: transfer mobility between velocity level at ground / track system interface and applied force

## Model main parameters



# Track work: test rig

## Laboratory test rig:

- **NF ISO EN 10846-2 implemented on whole tie (performance of resilient layer)**

- **setup for insertion loss**

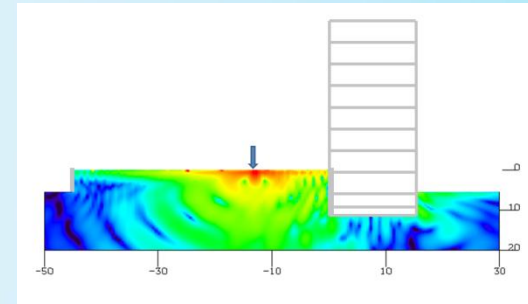
**CAE software and test rig used for Eurostar track work in London (SATEBA / CSTB); ongoing work for tramway tracks**



- CSTB / SNCF track department (2008)
- SNCF / RFF / CSTB / SATEBA on freight trains (VIBSOLFRET 2007-2008)



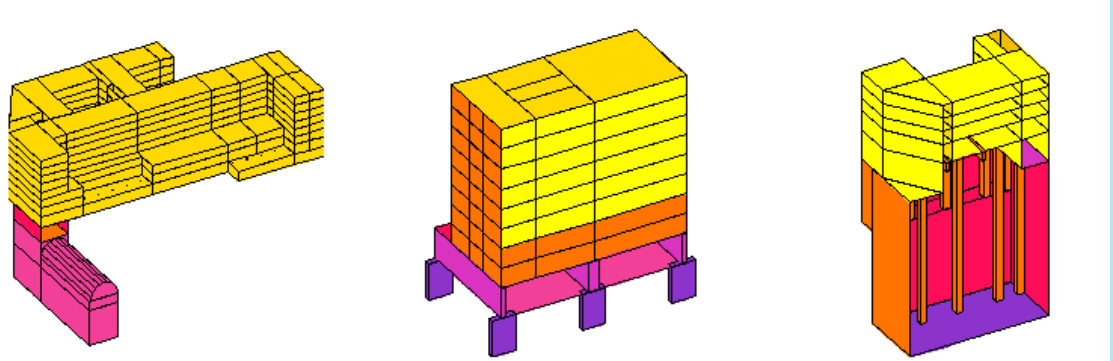
## Conclusions & perspectives



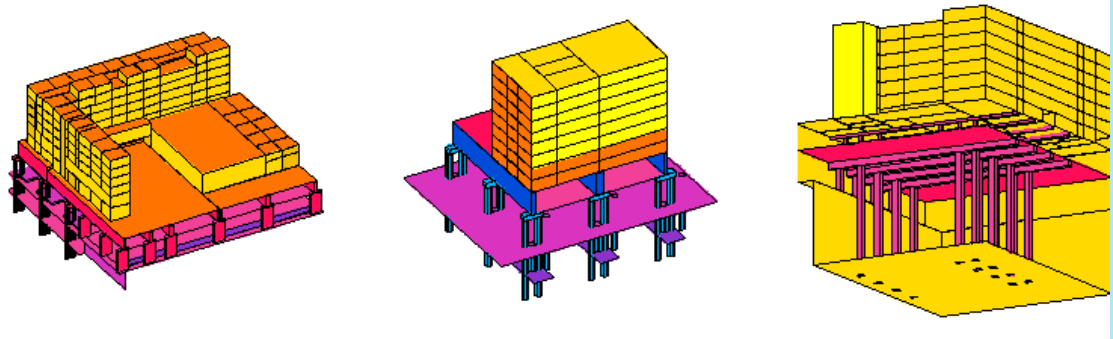
- SEA: valid for bending excitation above 50 Hz
- BEM/FEM approaches
- Source /receiver approach using mobilities: ground/foundation: BEM2.5D, (3D under way)  
building (upper structure) : commercial software (Nastran,...)
- Superstructure in 2D: results are sufficient for a parametric study
- Effect of structural modifications estimated : increase of data in empirical model (data base)
- Estimation of structure-borne vibration levels and ground borne noise levels in buildings
- Exposure descriptors for human perception included (post-treatment stage)  
=> expression of a relation between annoyance and structural parameters possible

# Examples of application : Large Projects in Paris

Eole



RERD



SEMAPA slab (Austerlitz)

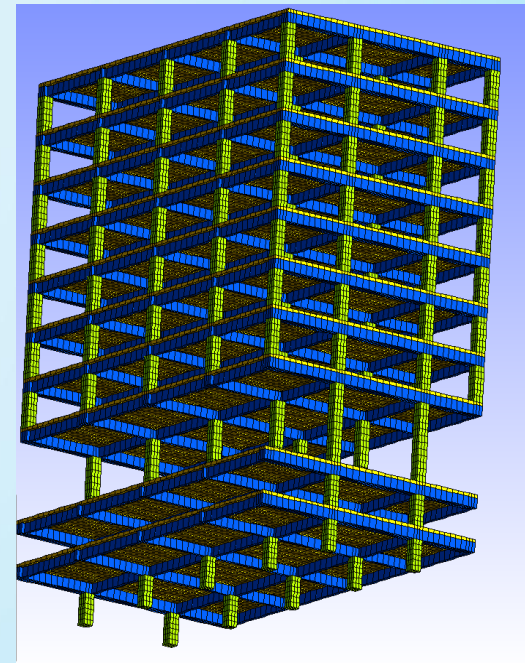
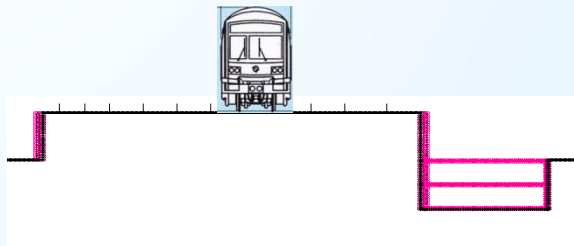
Structures above ground  
Structures above ground

SEA  
dedicated models (waves/SEA)



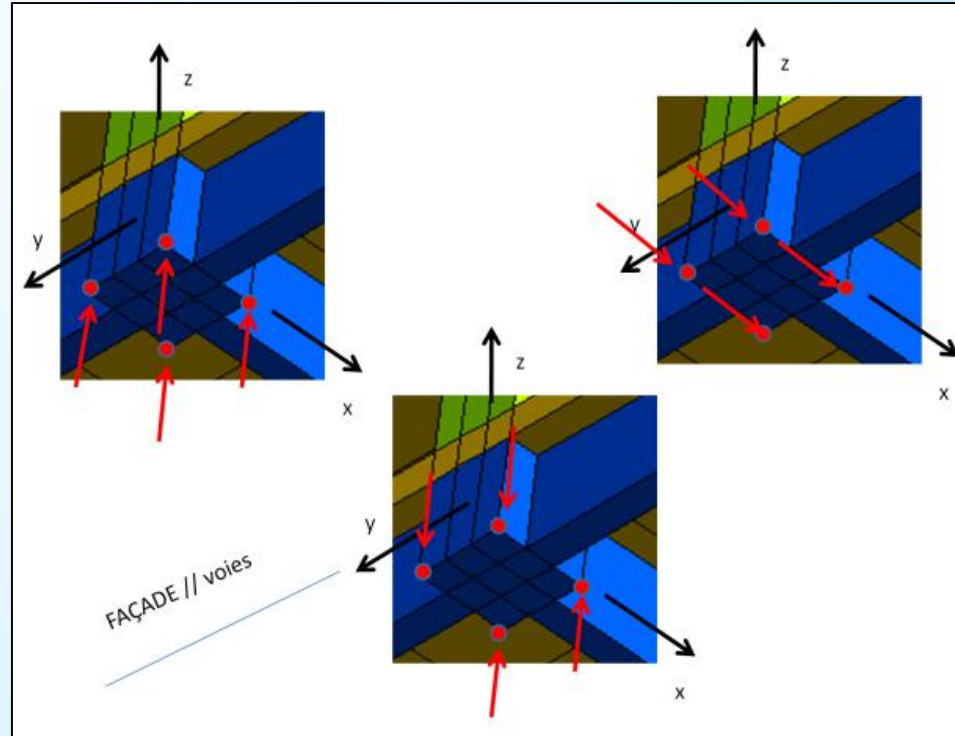


## Example of application: building close to a railway station (SNCF)



*Below ground (calculs BEM) and above ground (Nastran)*

# Example of application: Computation of mobilities

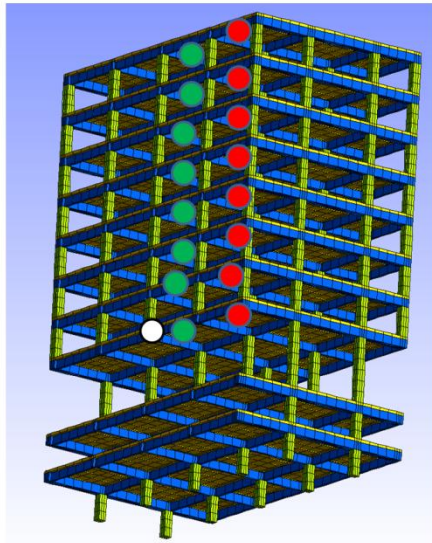


*Excitation at the lower part of a superstructure to compute mobilities*



# Example of application: floor response (bending)

- Excitation
- Colonne 1
- Colonne 2



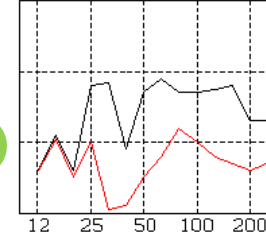
Excitation: horizontal

vertical



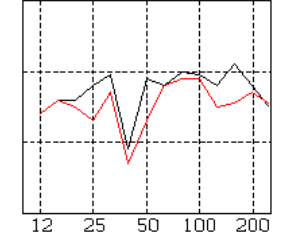
Column 1

Excit Hor col 1



Hz

Excit vert col 1

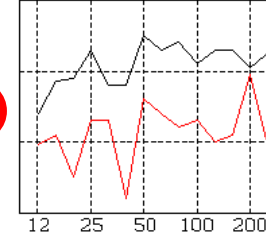


Hz

L<sub>V</sub> flexion de dalles  
10 dB / grad

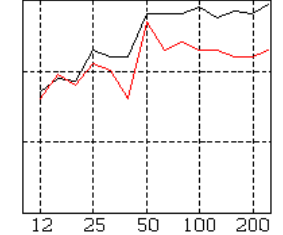
Column 2

Excit Hor col 2



Hz

Excit vert col 2



Hz

RDC

RDC+1



## Example of application: effect of structural modifications

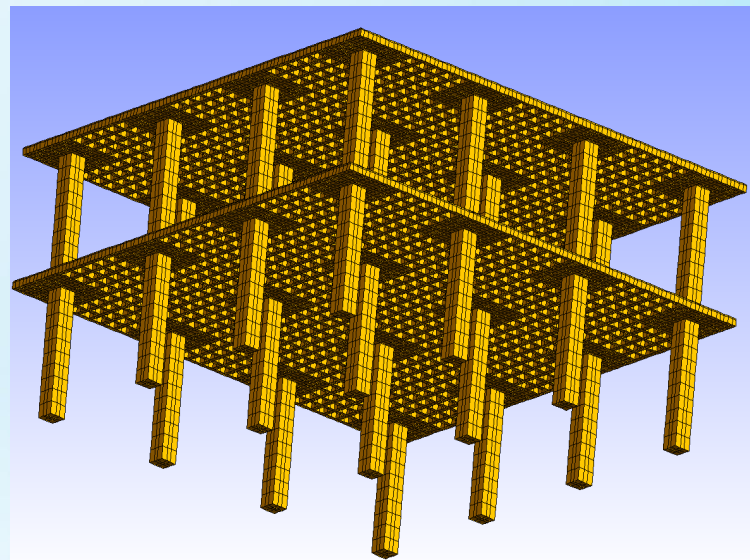
Project CSTB/ACOUPHEN

**Warehouse close to existing tracks: converted into lodgings (above top slab)**

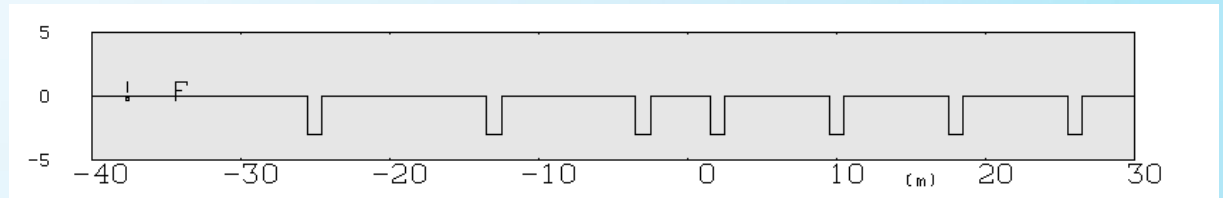
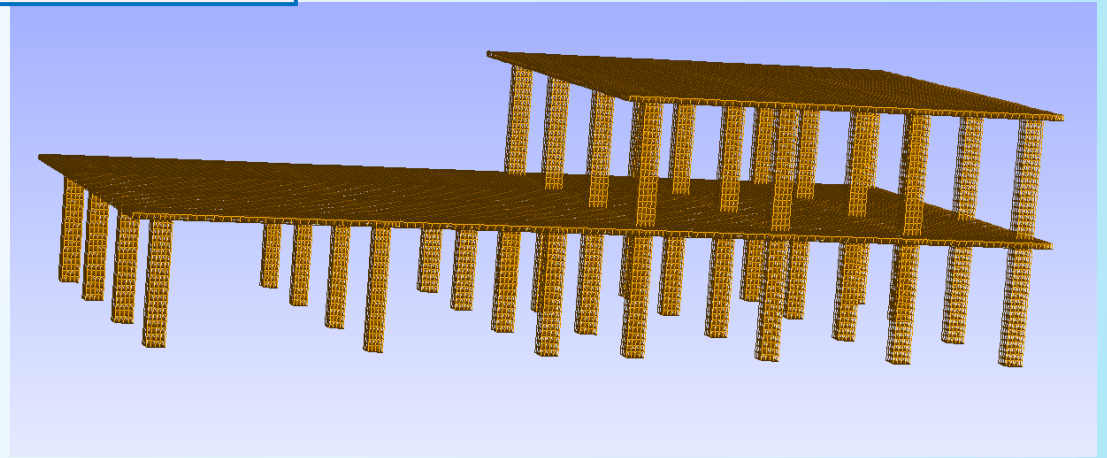
Velocity response measured: model calibration

**Objective:** predict the influence of structure modifications

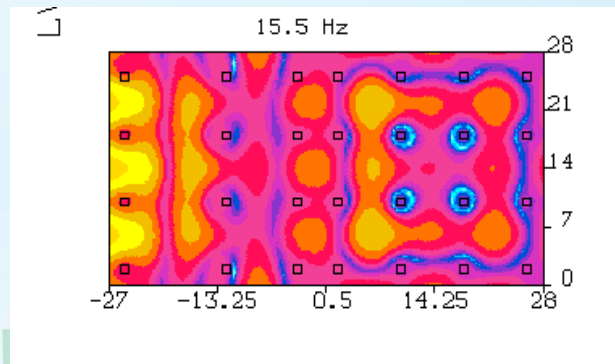
*Part of the existing  
geometry*



FEM model



BEM computation of Velocity at the top of foundations



Calculated Floor velocity Levels



